

## EXERCICE 1

Design of the steering system of an automobile, as it is shown in the figure.

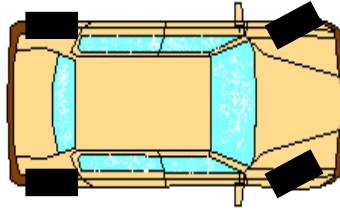


Figure E1.1.- Design of the steering system of an automobile.

Solution:

a) First requirements:

- Frontal steering system.
- Null yaw tyre angles .

b) Kinematic requirements:

- As figure E.2. shows, the correct motion of the car forces to  $\delta_i \neq \delta_e$ .

The ratio between  $\delta_i$  and  $\delta_e$  is the known “Proportion of Akerman”:

$$\text{Cot}(\delta_i) - \text{Cot}(\delta_e) = \frac{b}{L}$$

(ec.E1.1)

Where “b” is the wheel track of the car, and “L” is the wheelbase.

For an average car:

$$b = 1,74 \text{ m. ; } L = 3,67 \text{ m.}$$

Therefore:

$$\text{Cot}(\delta_i) - \text{Cot}(\delta_e) = 0,47411$$

(ec.E1.2)

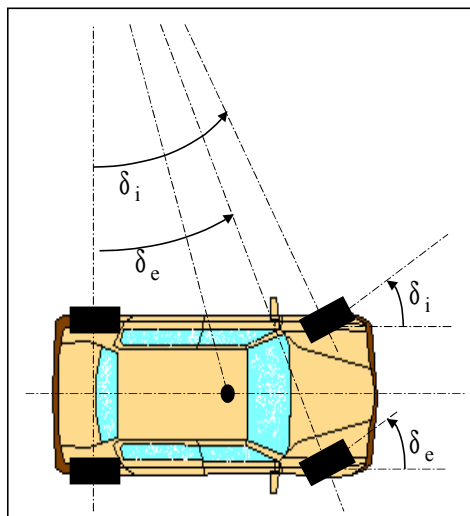


Figure E1.2.- Kinematic requirement for the right operation of the steering system.

c) Precision points.

We consider a car, where usually the steering angle takes values into the interval of  $\pm 20^\circ$ . Because steering system has a symmetrical motion, in order to start the synthesis of the mechanism it is considered an interval of values between  $0^\circ$  to  $20^\circ$  for the internal angle  $\delta_i$ .

Now the *Spaced of Chesbyshev* is applied, (see fig. E1.3 and E1.4):

$$\delta_{ij} = \frac{1}{2}(\delta_{if} + \delta_{ii}) - \frac{1}{2}(\delta_{if} - \delta_{ii}) \cos \frac{\pi(2j-1)}{2n}$$

With three precision points, the results for the internal steering angle are:

$$\delta_{i1} = 1.339745^\circ = 0.023382961 \text{ rad.}$$

$$\delta_{i2} = 9.999993^\circ = 0.1745328 \text{ rad.}$$

$$\delta_{i3} = 18.66024^\circ = 0.325682639 \text{ rad.}$$

For the external steering angle, applying the Proportion of Akerman, (ec.E1.2), the results are:

$$\delta_{e1} = 1.325058^\circ = 0.023126621 \text{ rad.}$$

$$\delta_{e2} = 9.242352^\circ = 0.161309478 \text{ rad.}$$

$$\delta_{e3} = 16.23025^\circ = 0.283271304 \text{ rad.}$$

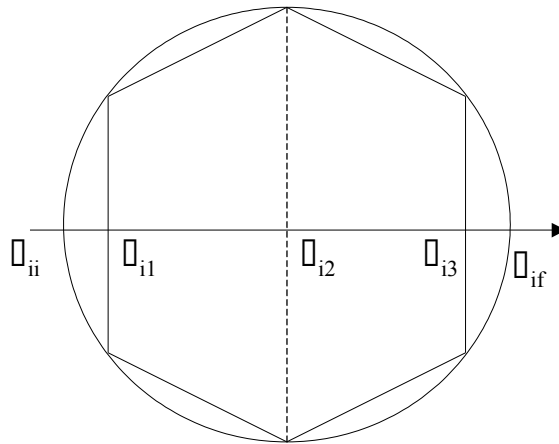


Figure E1.3.- Spaced of *Chesbyshev* with three precision points.

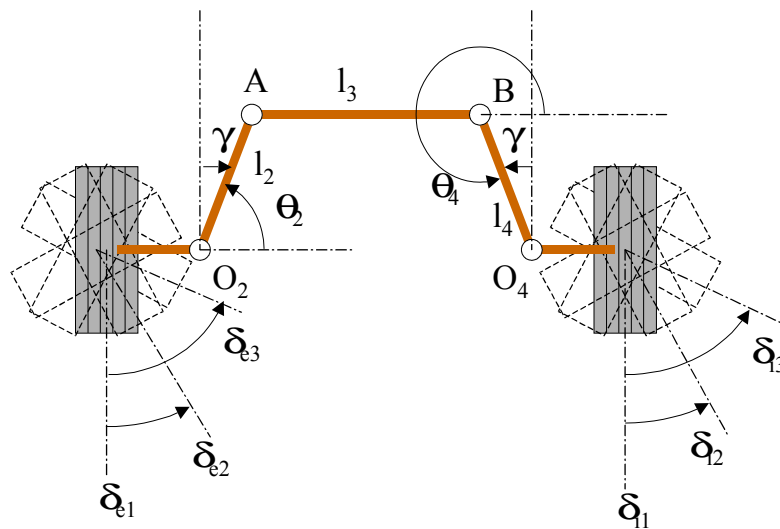


Figure E1.4.- Steering system scheme.

d) Synthesis de Bloch and Equation of Freudenstein.

In order to do the synthesis of the mechanism for the steering system, the angles  $\theta_2$ ,  $\theta_4$  are used, (see fig. E1.4 and E1.5):

$$\begin{aligned} \theta_2 &= \pi/4 - \gamma + \delta_e & \theta_4 &= 3\pi/4 + \gamma + \delta_i \\ \theta_{21} &= \pi/4 - \gamma + \delta_{e1} = 1.245 & \theta_{41} &= 3\pi/4 + \gamma + \delta_{i1} = 5.085 \\ \theta_{22} &= \pi/4 - \gamma + \delta_{e2} = 1.383 & \theta_{42} &= 3\pi/4 + \gamma + \delta_{i2} = 5.236 \\ \theta_{23} &= \pi/4 - \gamma + \delta_{e3} = 1.505 & \theta_{43} &= 3\pi/4 + \gamma + \delta_{i3} = 5.387 \end{aligned}$$

Where angle  $\gamma$  takes the value,  $\gamma = 0.34906585$  rad. =  $20^\circ$ .

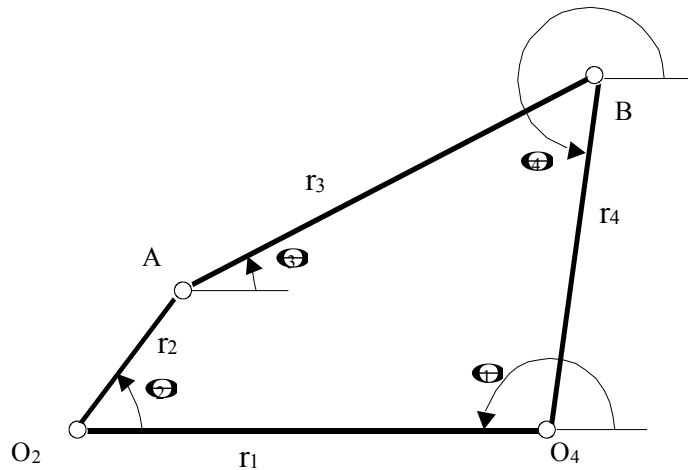


Figure E1.5.- Scheme of the mechanism.

Now is able to apply the Synthesis of Bolch, and Equation of Freudenstein.

$$K_1 \cos \theta_2 + K_2 \cos \theta_4 + K_3 = \cos(\theta_2 - \theta_4)$$

$$K_1 = \frac{r_1}{r_4} ; K_2 = \frac{r_1}{r_2} ; K_3 = \frac{r_3^2 - r_1^2 - r_2^2 - r_4^2}{2r_2r_4}$$

Using the before values of  $\theta_{2j}$ ,  $\theta_{4j}$ , a set of three equations with three unknowns  $K_1$ ,  $K_2$  and  $K_3$  is obtained:

$$K_1 \cos \theta_{21} + K_2 \cos \theta_{41} + K_3 = \cos(\theta_{21} - \theta_{41})$$

$$K_1 \cos \theta_{22} + K_2 \cos \theta_{42} + K_3 = \cos(\theta_{22} - \theta_{42})$$

$$K_1 \cos \theta_{23} + K_2 \cos \theta_{43} + K_3 = \cos(\theta_{23} - \theta_{43})$$

Calculating the values of  $K_1$ ,  $K_2$  and  $K_3$ :

$$K_1 = 8.062$$

$$K_2 = 7.973$$

$$K_3 = -6.249$$

The length of a bar 1 is chosen:

$$r_1 = 1 \text{ m.}$$

Then the length of the three remaining bars of a four bars mechanism are obtained:

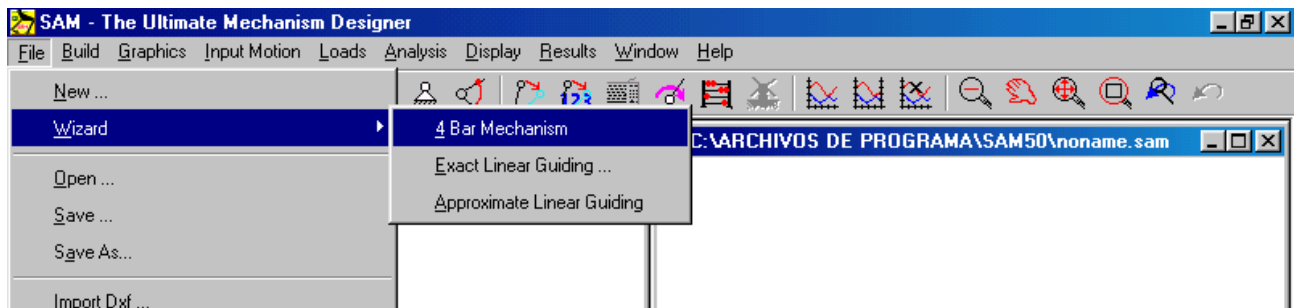
$$r_2 = 0.125 \text{ m.}$$

$$r_3 = 0.125 \text{ m.}$$

$$r_4 = 0.837 \text{ m.}$$

e) Synthesis of the mechanism using the computer program SAM PC v5.0:

We can test the before solution using computer programs, as SAM PC v5.0. This computer program provides a “Wizard” menu that can be used in order to apply synthesis of functions:



We choose the “4 Bar Mechanism” option. Then the following form appears:

Next step is to introduce the pairs of angles  $(\alpha, \beta)$ , and the coordinates of  $A_0$  and  $B_0$ ,

As it is considered in the section f) of this exercise, for the synthesis we have used the angles  $\theta_2, \theta_4$ , (see figure E1.5.) This implies:

$$\alpha = \theta_2$$

$$\beta = \pi - (2\pi - \theta_4) = \theta_4 - \pi$$

$$\alpha_1 = 71.3332603^\circ ; \quad \beta_1 = 111.349099^\circ$$

$$\alpha_2 = 79.2400796^\circ ; \quad \beta_2 = 120.000764^\circ$$

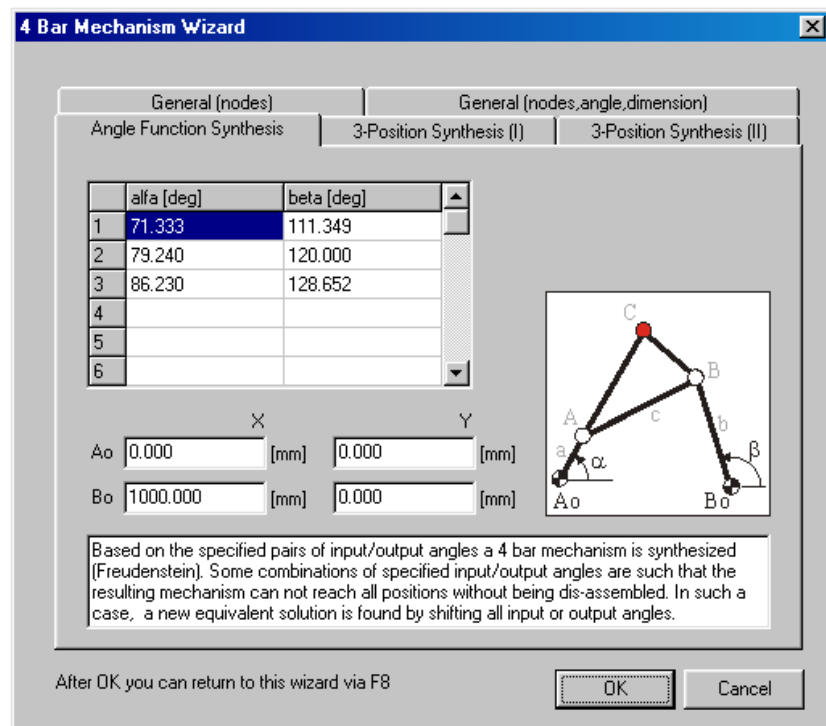
$$\alpha_3 = 86.2301661^\circ ; \quad \beta_3 = 128.652428^\circ$$

Also, in section f), we have chosen,  $r_1 = 1$  m. Consistently, we can adjust the following coordinates of  $A_0$  and  $B_0$ :

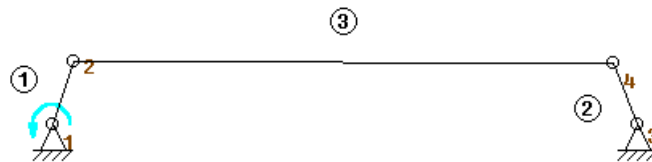
$$A_0 ( 0, 0) \text{ mm.}$$

$$B_0 ( 1000, 0) \text{ mm.}$$

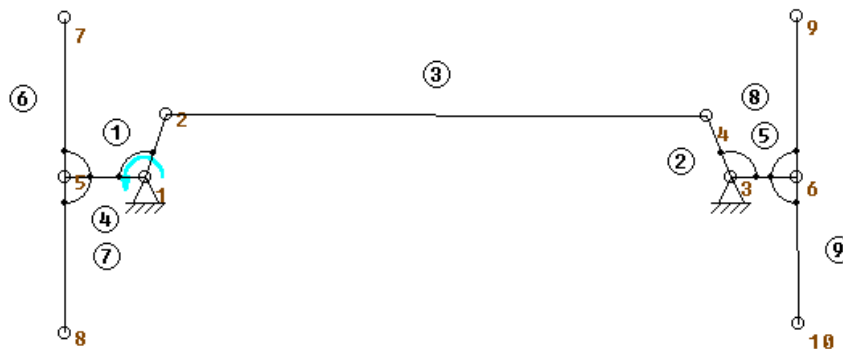
Now, we introduce all the before information in the form, as follows:



Then "O.K." is stroke, and it appears the solution:



We can complete the mechanism in order to design it more realistic than before:



The next figure shows the relation between both angles  $\alpha$  and  $\beta$

Graph of Selected items

